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# Self-sustained autonomous wireless sensing based on a hybridized TENG and PEG vibration mechanism

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#### ABSTRACT

Autonomous wireless sensor nodes (WSN) for information acquisition and status monitoring, play an important role in the boom area of the internet of things (IoT) and industry 4.0. Self-sustained power supply is an important pursuit in massive practical applications but yet to be developed. Here we propose a novel hybrid piezoelectric generator (PEG) and triboelectric nanogenerator (TENG) to form a novel self-sustainable WSN. The PEG consisting of a hinged-hinged PZT bimorph and two T shaped proof mass, has an output power of 6.5 mW excited in 25 Hz at 1.0 g. PEG also shows broadband characteristics thanks to the impact of the TENG and tunable frequency due to the axial force. 30 serial LEDs in sine vibration and 20 serial LEDs in shock vibration are lighted up with the proposed double voltage rectifier circuit by PEG, which can serve as alarming signals in vibration and drop monitoring. The triboelectric accelerometer shows good linearity with a sensitivity of 15 V/g in 0-1.5 g with an optimized gap of 1.5 mm. After low power design, Arduino nano and RF transceiver can be sustainably powered by PEG, and send the TENG acceleration signal wirelessly by Zigbee. A VR train monitoring demonstration has been conducted showing the great prospect of the self-sustainable WSN in harsh environments.

### 1. Introduction

Driven by rapidly developed internet of things (IoT) technology for harsh environment monitoring, self-sustained wireless sensor nodes (WSNs) are desired to remove the required labor-intensive task of changing the battery for WSNs in the remote area and harsh environment, where the battery lifespan is extended by energy harvesting technology [1-5]. Using the self-powered sensors based on the piezoelectric and/or triboelectric mechanisms have been investigated as promising solutions to reduce the power consumption of the whole WSNs [6–16]. More importantly, sizable energy collected from ambient and saved in the capacitor and/or battery is the ultimate approach to support the required power for the operation of wireless sensory data transmission of WSNs in the IoT framework [17-20].

There are many machines, robots, and devices used in remote area and harsh environments, such as drilling in mining, bridges, train rails, whose working status can be continuously monitored by embedded accelerometers, revealing the irregular vibration incidents where an abnormal acceleration value is detected. Status monitoring of various types of equipment[21], such as cars [22,23], train [24,25], pump [26], gearbox [27], and so on, especially relies on distributed WSNs using accelerometers. For example, the heavy haul railway has nearly 100 carriages and wheelsets. The wheelset bears continuous vibration in the range of < 2 g, 10–40 Hz during its operation [28,29]. Accelerometers

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can continuously monitor axle box vibration, and regularly report the acceleration levels as a WSN to the senor hub, e.g., the head of the train. When the abnormal sensor data is measured, which indicates the axial or bears need to overhaul or even in the broken situation, the alarm signal will be notified to the central control office at the station.

So far, the self-powered accelerometers have been reported by a few groups with various designs and mechanisms for different applications including healthcare, IoT, and harsh environment monitoring [30–35]. For instance, Liu et al. provided theoretical study and developed a selfpowered accelerometers with high sensitivity [36]. Shi et al. developed a self-powered gyroscope ball with a ball-shape design where the hollow sphere contains several steel balls inside to move freely on the inner surface for triboelectric output generation [33]. To achieve a broadband behavior, Gupta reported a hybrid energy harvester with a non-linear stiffing effect introduced by mechanical stoppers, where the TENG device is located for acceleration sensing [35]. For another instance, a selfpowered multifunction motion sensor with a magnetic-regulated TENG is reported, where the TENG consists of a free-standing magnetic disk on a PTFE plate, but with a limitation of in-plane accelerations and motion status detection [32]. A low-frequency (< 12 Hz) spring-mass system integrated with TENG is developed as a vibration accelerometer for railway state monitoring, but the minimal detected acceleration level is higher than 1 m/s<sup>2</sup> possibly due to the large gap between the triboelectrification layers in the structure [30]. Besides, the adjustable resonant frequency has rarely achieved with the reported designs. Complex signal acquisition circuits for signal processing of the TENG accelerometer could be power consuming, especially considering the power required for wireless transmission.

Energy harvesting technology then has emerged a promising solution to provide renewable and sustainable energy to power the WSNs. Despite renewable energy such as solar and wind has been developed and deployed outdoors successfully [37,38]. It is hard to get renewable energy from the dark and narrow space inside of most types of equipment, such as axial box and gear box. Luckily, there is wealthy vibration energy existing in various equipment during operation especially in low frequency band. Vibration energy harvesting can play an important role to supply electrical power for WSNs by piezoelectric [39], electrostatic [40], electromagnetic [41], and triboelectric [42] or their hybrid approaches [43-45]. Among them, piezoelectric and triboelectric approaches are reported with higher power density [46]. For example, a honeycomb structure inspired triboelectric nanogenerator is reported with a high power density of 50 W/m<sup>3</sup> (25 Hz, 2.0 mm vibration amplitude) [47] and a high output power of 227 mW has been achieved with a piezoelectric nanogenerator of small device size ( $\Phi$ 48 mm imes 27 mm) [48]. The design of mechanical energy conversion systems generally focuses on the frequency match with the ambient vibration to maximize the harvested energy at the resonant state.

The piezoelectric generators (PEG) mainly deploying a lead zirconate titanate (PZT) based monomorph and/or bimorph cantilever or beam in the centimeter-size range, where such fundamental mechanical transducers can convert transverse vibration into the longitudinal strain, and AC output is generated when the PZT cantilevers/beams are under vibration [17-20]. Usually, a proof mass is added to increase the mechanical energy and decrease the resonant frequency [49,50]. The stopper design is a practical method to achieve broadband characteristics and overload protection [51,52]. To increase the overall output power of the PEG, frequency-up-conversion mechanisms have been investigated and reported as well [53,54]. Besides, to compensate for the mismatch between device resonant frequency and excitation frequency, applying the axial force to the bulked beam has been proven to be an effective approach of frequency tuning. Adjust the axial force is an indirect and convenient approach to adjust the stiffness of the system due to it keep away from the moving part. Fixed or hinged beam can tuning the frequency by adjusting the screw rotation of the bolt [55]. Cantilevered piezoelectric beam with magnet tip mass can obtained different natural frequencies by adjusting the gap between the magnets [56]. The

combination of these technologies will bring more flexibility and adaptability to low-frequency and broadband vibration energy harvesting, leading to desirable performances for various applications [57–61].

Vibration-based triboelectric nanogenerator (TENG) aiming at lowfrequency vibration energy harvesting has been studied [62–64]. For example, Bhatia et al. has reported a tandem TENG for scavenging mechanical vibrational energy with vertical contact-separation mode [65]. Shi et al. reported a triboelectric buoy ball harvesting vibrational energy from ocean waves working on the sliding mode [66] A hybridized TENG and PEG vibration mechanism will combine advantages of high voltage in TENG and high current output in PEG. Most previous works of the hybrid generators are only used for harvesting energy to enhance the output power [48,60,67–72] or for multifunctional sensing [31,73–75]. However, direct parallel or series connection of the TENG and PEH would cause the mismatching of the impedance between them. In this regard, it is more reasonable to separately utilize the outputs of the TENG and PEG in the vibration system.

Self-sustained WSNs are very crucial for IoT applications in remote areas and harsh environments. The sustainable power supply required for the microcontroller unit (MCU) and radio frequency (RF) transceiver is typically at a few milliwatt level of power consumptions. It still remains a great challenge for the realization of the self-sustained autonomous WSN. Wen Feng et al. proposed a novel approach to realize the direct wireless transmission of the triboelectric sensory information requiring no external power, by simply combining a TENG textile, a mechanical switch, and a coil to form an RLC circuit [76]. Secondly, with the aid of the low power consumption BLE module, He et al. demonstrated a self-sustainable healthcare monitoring system for temperature and humidity sensing, powered by scavenged energy from foot motions through TENG textiles [77]. Although some commercial WSNs have very low power consumption at the microwatt level, such as Bluetooth temperature and humidity sensors, which are commonly used for TENG or PEG energy harvesting applications [18,78], there is still a mismatch between the output power of nanogenerators and device power consumption. Therefore, in most cases, it requires a long time for the PEG or TENG to charge up a capacitor with energy high enough to power the WSNs, due to the large gap between the output power and operation power. As such, the operation of the self-sustained WSNs is yet to be really sustainable for most of the hardware solutions. To address this issue, duty cycle design should be implemented to make WSN have shorter operation time and longer rest time to reduce average power consumption, which may realize the programmable and reconfigurable WSNs.

In this paper, we present a novel hybrid generator and propose a selfsustained WSN based on a hybridized TENG and PEG vibration mechanism. The hybrid nanogenerator is thoroughly investigated by simulation and experiments to achieve broadband behavior and tunable resonant frequencies. The TENG functioning as the self-powered acceleration sensor is also optimized to achieve a good sensing performance. The Arduino-based programmable accelerometer WSN is designed in a low power consumption style. In the self-sustainable WSN, the TENG output as the acceleration sensing signal is fed into the MCU, while the PEG sustainably supplies power to the MCU and RF transceiver to transmit the acceleration signal out wirelessly in diversified IoT applications as shown in Fig. 1(a).

#### 2. Structure and working mechanism

The structure design of the proposed hybrid generator is shown in Fig. 1(b), in which the device consists of one PEG and two TENGs. A PZT bimorph is hinged-hinged mounted. Two T shaped copper proof masses are bonded with the PZT bimorph by foam, which can reduce concentrated stress. The cube package material is polymethyl methacrylate (PMMA). The bolt and nut mounted at one side of the cube package can give an axial force to tune the resonant frequency of PZT bimorph. Two



Fig. 1. (a) Schematic illustration of autonomous WSN for equipment vibration monitoring. (b) Structure design of hybrid TENG and PEG module. (c) Working principle of PEG. (d) Working principle of TENG.

TENGs function as the stoppers for PEG overload protection and generate signals in contact-separation mode. Fig. 1(c) shows the deformation of the PZT bimorph as the working principle of PEG. Excited by ambient vibration, the transverse inertial force of proof mass will induce longitudinal strain in PZT bimorph. Due to the d31 piezoelectric effect, an alternating current will be generated in a parallel connection of two piezoelectric layers, and the polarization direction of the piezoelectric layers is from bottom to top. Fig. 1(d) shows the "contact-separation" working principle of TENG. A nickel fabric as a positive electrode is bonded with copper proof mass for a moving part. Eco flex with pyramidal synaptic array structure is selected as the negative triboelectric material for its soft stiffness and sufficient contact to generate more triboelectric charges. The flat side of eco flex is bonded with PMMA by another nickel fabric as a negative electrode for the substrates.

The schematic diagram of the working cycles of the hybrid generator is shown in Fig. S1. When contact occurs, the negative triboelectric charges are transferred from the nickel fabric on the proof mass to eco flex. In the sine excited state, PEG will vibrate and PZT will generate sine voltage signal accordingly. The separation between TENG will also generate a sine voltage signal due to electrostatic induction. The two TENGs located above and below the proof mass operate in the opposite phases.

To further elucidate the contribution and the creative engineering design of this work clearly compared to the current self-sustainable wireless IoT systems, we have summarized some recent works in Table 1 as shown below. For most of the reported works, the systems consist of the developed energy harvesters and commercial sensors (e.g., temperature sensor, humidity sensor, accelerometer) in two separate sections. For example, He et al. developed a triboelectric-piezoelectric-electromagnetic hybrid nanogenerator as the power source of a self-powered wireless monitoring system, which detects the acceleration and temperature of the hybrid nanogenerator by the integrated commercial sensors on the circuit board [48]. Similarly, Jin et al. proposed a self-powered wireless sensor based on a vibrational hybrid nanogenerator and a commercial temperature/humidity sensor board for the

train monitoring system [24]. However, the vibrational status of the nanogenerator, which is considered as an essential characteristic to reveal the proper functionality of the train, isn't taken into account in their system. Recently, Khan et al. developed a wireless sensing system realized with an all-in-one TENG, i.e., the device consists of multiple TENGs with one of them serving as an oscillation frequency sensor and the others functioning as power sources [79]. Though the wireless sensing system has a high integrity, the sensing function is limited to the vibrational frequency and with poor linearity from 10 Hz to 60 Hz. In our self-sustainable WSN, we integrate the PEG and TENG in a single device with the PEG harvesting energy from the external vibration and the TENG monitoring the acceleration of the external stimuli, without the need to introduce commercial sensors to the whole system. Besides, good linearity has been achieved with the TENG sensor in a sensing range up to 1.5 g through the structure optimization. Moreover, the adjustable stopper distance and the axial force endows the device a good adaptability to different ambient environment aiming at diversified applications as illustrated in Fig. 1.

Moreover, compared with the silicon-based capacitive accelerometer, the triboelectric accelerometer does not need an additional power supply. The self-power piezoelectric accelerometer has low sensitivity in low-frequency detection and requires the charge amplifier. The sensitivity of the self-generating signal of the triboelectric accelerometer is very high even under low-frequency excitation, which can reach tens of volts or even up to 100 volts. Moreover, the triboelectric accelerometer is advantageous in terms of low cost, easy assembly, and the simple subsequent signal processing circuit. The limitation of the triboelectric accelerometer is that the resolution is low and the vibration waveform has poor tracking performance at current states. In this case, the triboelectric accelerometer is more suitable for vibrational amplitude monitoring or shock counting.

# 3. Design and performance of PEG harvester

PEG is firstly designed by finite element analysis (FEA) in COMSOL.

teview of	recent self-sustainable wireless IoT.					
Ref.	Device features	Power source	Sensing mechanism	Application	Volume	Charging
[20]	Triboelectric-electromagnetic hybrid	Peak power: TENG (0.36 mW) EMG (18.6 mW)	Commercial temperature and humidity	Self-powered wind speed sensing	$10  imes 8  imes 6  ext{ cm}^3$	1 mF 20 V
	nanogenerator (powering)	at wind speed of 9 m/s	sensor		(estimated)	30 s
[48]	Triboelectric-piezoelectric-electromagnetic	Peak power: TENG (78.4 µW)	Commercial temperature sensor and	Vibration and temperature	$\Phi4.8 imes2.7 ext{ cm}^3$	1 mF 8 V
	nanogenerator (powering)	EMG (36 mW and 38.4 mW)	triaxial accelerometer	monitoring		250 s
		PEG (122 mW and 105 mW) at 20 Hz				
[24]	Triboelectric-electromagnetic nanogenerator	Peak power: TENG (0.34 mW/g) EMG	Commercial temperature and humidity	Self-powered temperature and	$\Phi4 \times 3 \text{ cm}^3$ (estimated)	4.7 mF 3 V
	(powering)	(0.12 mW/g)	sensor	humidity sensing		22 s
[62]	Triboelectric nanogenerators (powering and	Peak power: TENG (10 mW)	TENG vibration sensor	Self-powered vibrational	$6.5 imes 6.5 imes 2~{ m cm}^3$	1 mF 3 V
	sensing)			frequency sensing		110 s
[80]	Rotating triboelectric nanogenerator (powering and sensing)	RMS power: TENG (44.4 $\mu$ W) at 300 rpm	TENG speed sensor	Self-powered wind speed sensing	$\Phi 10  imes 1.6~{ m cm}^3$	0.1 mF 5 V 15 s
[81]	Triboelectric-electromagnetic nanogenerator	Peak power: TENG (15.21 $\mu$ W) EMG	Commercial temperature sensor	Self-powered temperature sensing	$16.7 imes 10 imes 4~{ m cm}^3$	0.1 mF 3 V
	(powering)	(1.23  mW)				200 s
This	Piezoelectric (powering) and triboelectric	RMS power: TENG (3.07 $\mu$ W) PEG (6.5 mW) at	TENG acceleration sensor	Self-powered acceleration sensing	$7 imes3 imes2.9~{ m cm}^3$	1 mF 20 V
work	(sensing) nanogenerator	25 Hz 1.0 g				25 s

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The modal analysis will show the first eigenfrequency of the PEG. The mass of the vibration system has a great effect on eigenfrequency. The T shaped proof mass consists of a small cube mass with length of 10 mm and a big cube mass with length of 50 mm. The separation of 3 mm between big cube mass and PZT is equal to the sum of the thickness of the small cube mass and the thickness of the foam, which ensures the moving space of the PZT bimorph. Since the mass largely affects the system eigenfrequency, the big cube mass thickness can be changed to tune the system eigenfrequency in the design phase. Fig. 2(a) shows the curves of first eigenfrequency change with different big mass thickness. Indeed, increasing the big cube mass thickness will decrease the first eigenfrequency. An appropriate mass thickness can be chosen to match the resonant frequency with the vibration of equipment where the PEG is mounted. In this research, the big cube mass thickness is set to 5 mm to match 25 Hz equipment vibration.

Stress check is our main concern in the frequency response analysis. Displacement and the stress nephogram in 25 Hz at 0.5 g are obtained by the dynamic analysis as shown in Fig. 2(d), and the part of PZT surface stress and deflection are shown in Fig. 2(e, f). The bonding edge of foam and PZT layer has the maximum PZT stress. Soft foam bonding can avoid stress concentration at the bonding edge. The center of the beam has the maximum deflection.

The curves of maximum PZT stress and open-circuit (load resistance of 1 M $\Omega$ ) voltage with different accelerations in 25 Hz as shown in Fig. 2 (b). Both of them increase linearly when the acceleration level increases. Although the higher the stress, the higher the output voltage, the maximum stress should be limited to the allowable stress to avoid material cracking. The allowable stress of the PZT ceramics is 80 MPa. Ceramic cracks will occur and the power generation performance will be reduced if the maximum PZT stress exceeds the allowable stress.

As shown in Fig. 2(c), the maximum PZT stress increases linearly with the vibration displacement of proof mass. To avoid the excessive stress applied to the PZT, the TENG can be set on top and bottom of the proof mass as a stopper to limit the vibration displacement within 2.2 mm, which is the boundary displacement for allowable stress. The distance between proof mass and eco flex is considered as the stopper distance. This research selects 3 different kinds of stopper distance, 1.0 mm, 1.5 mm, 2.0 mm, respectively in prototype performance experiments.

Fig. 2(g) shows the experiment results of frequency response voltage (load resistance of 1 M $\Omega$ ) curves of PEG with different stopper distance ds = 1.0, 1.5, 2.0 mm. The resonant frequency is near 25 Hz and the phenomenon of clipping peak appears near the resonant frequency. The stiffness becomes sharply harder when PEGs impact with TENG (Fig. S2), and the nonlinear extension of frequency band occurs. Broadband behavior is achieved thanks to the TENG as the stopper. PEG with ds = 1.0 mm has a wider broadband range but lower voltage output. PEG with ds = 2.0 mm has a narrower broadband range but higher voltage output. The bigger the acceleration level, the wider broadband range. For PEG with ds = 1.0 mm, the band for normal operation of TENG in 1.0 g acceleration is 21-28 Hz and 20-30 Hz in 1.5 g acceleration.

Despite big cube mass thickness can be changed to tune the system eigenfrequency in the design phase, there will be some mismatch between the actual excitation frequency and the resonant frequency of PEG prototype. Therefore, an axial force is applied to tune the resonant frequency of PEG. A theoretical model and analysis is provided in Note S1. Eq. (1) indicates the relation between axial force *P* and the open-circuit resonant frequency  $f_r$  of PEG. As shown in Fig. 2(h), screw nut connection is applied at one side of the hinged supporter. The axial stress can be estimated by screw rotation (Note S2). Eq. (2) indicates the relation between screw rotation angle  $\theta$  and the axial force P. PEG resonant frequency tuning under different axial forces is shown in Fig. 2(h). It can be observed that the PEG resonant frequency decreases from 25 Hz to 19 Hz along with the axial force varies from 0 N to 12 N.



**Fig. 2.** Design and analysis of PEG in COMSOL (a) First eigenfrequency with different big mass thickness. (b) PZT maximum stress and voltage under different acceleration. (c) PZT maximum stress with different displacement. Vibration analysis in 0.5 g acceleration at 25 Hz: (d) first resonant modal, (e) stress on the surface of PZT and (f) deflection along the beam in resonant state. Broadband vibration when TENG impacted: (g) experimental frequency response voltage curves of PEG with different dis = 1.0, 1.5, 2.0 mm under acceleration of 0.5, 1.0, 1.5 g. (h) PEG resonant frequency tuning under different axial force: (I) Schematic diagram; (II) Experimental frequency response voltage curves of PEG with ds = 1.5 mm under acceleration of 1.0 g; (III) Comparison of theoretical and experimental results.

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$$f_r = 2\pi \sqrt{\left(1 - \frac{P}{P_{cr}}\right) \frac{\pi^4 EI}{2L^3} / \left(M + \frac{m}{2}\right) \left(1 - k_e^2\right)}$$
(1)

Where  $P_{cr}$  is the Euler critical buckling load, *EI* is the bending rigidity of the beam, *L* is the beam length, m is the beam mass, *M* is the proof mass, and  $k_e$  is the electromechanical coupling coefficient.

$$P = \frac{EAp_s\theta}{2\pi L} \tag{2}$$

Where EA is the compressive stiffness of the beam,  $p_s$  is the screw distance.

# 4. Design and performance of the TENG acceleration sensor

According to the acceleration sensing mechanism of TENG, the stopper distance *ds* affects the range and linearity of the triboelectric accelerometer, which should be discussed and investigated. The stopper distance in the prototype can be controlled by the height of the two hinged supporters. In the vibration experiment at a fixed frequency of 25 Hz, hybrid generators with three kinds of stopper distance are tested in 6 acceleration levels, i.e., 0.25 g, 0.5 g, 0.75 g, 1.0 g, 1.25 g, and 1.5 g, respectively, where the 1.0 g equals to 9.8 m/s<sup>2</sup>. Their time response voltage curves are shown in Fig. 3(a). The amplitudes of two TENG signals both increase as the acceleration level arises. The amplitude of PEG signal increases with the acceleration first but quickly saturates to the maximum value due to the limitation of the TENG stopper distance. For the stopper distance of 1 mm, the PEG signal keeps stable

as acceleration level arises beyond 0.5 g, with TENG output of 18 V and PEG output of 32 V at 1.5 g. For the stopper distance of 1.5 mm, the PEG signal keeps stable as acceleration level arises beyond 0.75 g, with TENG output of 23 V and PEG output of 42 V at 1.5 g. For stopper distance of 2 mm, the PEG signal keeps stable as acceleration level arises beyond 1.0 g, leading to TENG output of 30 V and PEG output of 47 V at 1.5 g. It is noted that a small stopper distance will limit the output of TENG and PEG, but a large stopper distance will cause no impact to the TENG at low acceleration levels and may cause the overload of the PEG. Therefore, the hybrid generator with the stopper distance of 1.5 mm is an optimal choice considering the large outputs from both TENG and PEG and the prevention of overload of the PEG.

To calibrate TENG as an accelerometer, Fig. 3(b) shows the rectified filter signal process of TENG. Here, TENG stopper distance of 1.5 mm excited in the acceleration of 1.0 g. TENG1 and TENG2 have similar sinusoidal signals with the same frequency but different phases. Therefore, they should be rectified by a rectifier (DF-10) separately before parallel connection. To get a stable direct current (DC) signal, a filter capacitor  $C_F$  of 1.3 nF is used. Fig. 3(c) shows the rectified filter TENG voltage at different accelerations in 5 min. They have very narrow drift without overlapping and can be identified easily with a high sensitivity of 15 V/g in 0–1.5 g. For accelerometer reading circuit, the voltage range of analog port in Arduino is within  $\pm$  5 V. Therefore, the load resistance of 6 M $\Omega$  is applied to limited TENG voltage to that range. Finally, voltage values of each TENG with different stopper distance at 6 acceleration levels are drawn in Fig. 3(d). It can be observed that TENG voltage signal with a stopper distance of 1.5 mm has the optimal linearity with the acceleration levels. Therefore, the 1.5 mm distance is



**Fig. 3.** (a) Experiment results: time response voltage curves of TENG1, TENG2, PEG with different ds  $= 1.0 \ 1.5 \ 2.0 \ mm$  under different accelerations at 25 Hz. (b) Rectified filter signal process of TENG by circuit (III): original signal of TENG1 (I) and TENG2 (II) are rectified separately before parallel connection (IV) and then filter as a stable signal (V). (c) Acceleration calibration curve of TENG accelerometer with ds  $= 1.5 \ mm$ . (d) Arduino analogy voltage curve of TENG accelerometer with different stopper distance.

desirable for both energy harvesting and acceleration sensing in the hybrid system. The discussion of the acceleration sensing mechanism and parameter optimization contribute to the design of the TENG accelerometer.

### 5. Application of PEG

PEG with broadband and adjustable resonant frequency can be used in energy harvesting at fixed frequency with small frequency drift or shock excitation. RMS voltage at the load resistance is get by a rectified filter interface circuit. RMS power is calculated by  $P_{RMS} = V_{RMS}^2/R_L$  . Fig. 4(a) shows RMS voltage and power response curves of TENG (TENG1 and TENG2 regulated before parallel connection) at different load resistances under a sine acceleration of 1 g at 25 Hz. Fig. 4(b) shows those of PEG. The maximum RMS power of TENG is 3.07  $\mu$ W at optimal load resistance of 33 MΩ. The maximum RMS power of PEG is 6.5 mW at optimal load resistance of 40 k $\Omega$ . This is a pretty good output compared to the published performances of low frequency PZT piezoelectric energy harvesters (Table S2). Since the maximum RMS power of PEG is almost two thousand times that of TENG under the same excitation conditions, PEG is more suitable to be an energy harvester due to the mW level power output and TENG is preferable to be a self-powered accelerometer due to the good sensing linearity.

Fig. 4(c) shows PEG charge curves of different capacitors under 1 g acceleration at 25 Hz. It can charge a capacitor of 330  $\mu$ F to 26 V quickly in 20 s. It is hopeful to supply power for many electronic devices. To increase the voltage amplitude, a double voltage rectifier circuit is designed in this work, as shown in Fig. 4(d). Compared to rectifier circuit, the negative end of the PEG and an alternating current (AC) terminal are short circuited in double voltage rectifier circuit. The AC voltage curve from - 30–30 V is then translated into a DC voltage curve from 0 V to 60 V, with an improvement of 100% compared to the conventional rectifier circuit with a DC voltage curve from 0 V to 30 V. After a double voltage rectifier circuit, the PEG can light up 30 LEDs in serial

connections under 1 g acceleration at 25 Hz.

The bigger acceleration, the higher PEG output voltage, the more LEDs in serial connection can be light on. Base on that, the alarm acceleration level can be directly set as the number of LEDs in serial connection. When PEG is excited below the alarm acceleration level, no LEDs will be light up. When PEG is excited beyond the alarm acceleration level, LEDs will be light up flashing light to transmit the alarm signal.

Besides sine vibration detection, an SOS shaped 20 LEDs in serial connection is developed in shock-based vibration detection, as shown in Fig. 4(e). Attenuated oscillation waveform with peak voltage of 50 V is shown after a double voltage rectifier circuit. It can flash SOS LED sign in every shock excitation. This can be utilized in landslide, cargo, or human drop monitoring.

# 6. Self-sustained autonomous wireless sensing

Despite TENG has shown good linearity as a self-powered accelerometer and PEG has shown the milli-watt level power output, there are still some works to do to achieve a self-sustained autonomous wireless sensing system. It includes the low power consumption design and the power management circuit design. The IoT application topology is shown in Fig. 5(a–c). The autonomous WSN consists of a hybrid generator, an LTC-3588-1 based power management circuit, two energy storage capacitors, an Arduino nano development board as MCU, and a DL-20 CC2530 A as RF transceiver. The host computer consists of a DL-20 CC2530 B as an RF transceiver, a USB to TTL serial port as an interface converter, and a laptop to show the received wireless signal. The communication between autonomous WSN and host computer base on the Zigbee in IEEE 802.15.4 international standard. It is a low power communication with a physical wireless range of 10–20 m.

The autonomous WSN circuit design is depicted in Fig. 5(b). The PEG provides AC voltages to PZ1 and PZ1. It has a 2.7–20 V input operating range and will be rectified and filtered in  $V_{in}$  and stored in capacitor  $C_{in}$ 



**Fig. 4.** RMS voltage and power response curves at different load resistance under 1 g acceleration at 25 Hz (a) PEG regulated, (b) TENG1 and TENG2 regulated before parallel connection. (c) PEG charge curves of different capacitors under 1 g acceleration at 25 Hz. (d) Double voltage rectifier circuit (III) for PEG to light up 30 LEDs (V) in serial connection under 1 g acceleration at 25 Hz; (I) original signal of PEG; (II) conventional rectified signal; (IV) double voltage rectified signal. (e) impulse signal of PEG to light up alarm LEDs.



**Fig. 5.** Demonstration of self-sustained autonomous wireless sensing system: (a) Schematic showing the connection and function of the components in the wireless sensing system. (b) Autonomous WSN circuit design. (c) IoT application topology. (d) Current consumption curve of MCU and RF in low power consumption mode. (e) Voltage curves of capacitor charging in LTC3588-1; (f) VR demonstration of monitoring status of the train, and wireless acceleration data stream received in serial port software on the host computer.

of 1 mF. When 3.3 V output in  $V_{out}$  is selected, under-voltage lockout (UVLO) in the chip will work from 3.67 V to 5.05 V. Capacitor  $C_{out}$  of 1 mF is utilized to stable load voltage to power Arduino nano in case of instantaneous large discharge. TENG1 and TENG2 are rectified and parallel connected, and a filter capacitor  $C_F$  of 1.3nF and an adjust resistance  $R_A$  of 6 M $\Omega$  are parallel connected to give a stable and suitable voltage signal. The voltage difference in A0 and A1 is linearly proportional to the amplitude of acceleration. The code in Arduino nano (Note S3) will read the analog port voltage and convert it into a digital signal to be sent to the RF transceiver.

Low power consumption design is of crucial importance in a selfsustained system. The current consumption curve of MCU and RF in normal operation mode indicates an average current of 33 mA (MCU 3 mA and RF 30 mA) in 5 V power supply (Fig. S5). Such 165 mW power consumption is far beyond the transit output power capability of the PEG. Therefore, the hardware and the program are modified into low power consumption mode. The low dropout regulator (LDO) and power LED in Arduino nano are removed, the input voltage can be decreased from 5 V to 3.3 V and additional current consumption of 2 mA in Arduino nano will be avoided. The current consumption of RF transceiver accounts for a large proportion. Only intermittent power supply can reduce average power consumption. Therefore, a 16 s sleep mode is set in every duty by coding in Arduino nano. D0 is also set to high of 3.3 V to supply power for RF transceiver in 0.2 s work and set low to

power off for RF transceiver in 16 s sleep. The current consumption curve of MCU and RF in low power consumption mode is shown in Fig. 5 (d). Such a low duty cycle of 1.2% can ensure a low average current consumption of 1.17 mA in 3.3 V voltage supply.

Voltage curves of capacitor charging in LTC3588-1 by PEG in 1 g acceleration at 25 Hz for self-sustained autonomous wireless sensing are shown in Fig. 5(e). UVLO will allow  $V_{in}$  reaches 5 V before charge  $V_{out}$  into 3.3 V.  $V_{out}$  is stable at 3.3 V from 10 s and  $V_{in}$  reaches 13.5 V at 40 s, the power switch of WSN is turned on manually. Although the slow drop in  $V_{in}$  for startup power consumption and quickly drop in  $V_{in}$  for RF and TENG sensor work power consumption of 0.2 s,  $V_{in}$  will keep arising in a sleep period of 16 s. The overall upward trend of  $V_{in}$  shows that the self-power system is sustainable.

In future, we plan to apply this WSN for abnormal vibration monitoring of various equipment, such as drilling in mining, bridges, and train rails, whose working status can be continuously monitored by embedded accelerometers, revealing the irregular vibration incidents where an abnormal acceleration value is detected. To illustrate the feasibility of such applications, we created a virtual reality (VR) environment where a visual train is moving continuously with accelerometers embedded in each cabin for its status monitoring. A visualization panel with four LEDs corresponding to each cabin is built up in the operation room, which indicates the working status of the moving train intuitively based on the detected sensing signals from the accelerometer. Supplementary Video 4 shows the application of train monitoring with our self-sustainable WSN that functions as the self-powered accelerometer in cabin 3 in the VR environment.

Supplementary material related to this article can be found online at doi:10.1016/j.nanoen.2020.105555.

In the practical testing, we use the vibrational shaker to generate vibration source with a set-up frequency and acceleration to mimic the vibration of a moving train. The TENG acceleration sensing signal will be sent by RF transceiver and received on the host computer. The acceleration data stream received in serial port software is shown in Fig. 5 (f). The bigger received data, the heavier vibration acceleration state. The acceleration data threshold can be set in the program to indicate the state of the vibration. Here, the received data is categorized into three ranges: below 200 (< 0.5 g), between 200 and 500 (> 0.5 g), and above 500 (> 1.5 g), which correspond to three working status: normal, alarm, and overload.

The VR environment for train monitoring is presented in Fig. 5(f), in which the WSN is mounted on the axial box of the train to keep track of the vibration status of it. Correspondingly, there will be a display panel in the main control room indicating the detected status of the train. Here we have built a virtual train with four discrete cabins, and the WSN that is mounted on the testing shaker is set as the acceleration sensor in cabin 3 in the virtual space. The vibration status of the testing shaker stimulates the real vibration of the moving train, which can be intuitively observed from the light color of the display panel. To mimic the real applications, the vibration acceleration of the train will be increased by wear and crack of shafting, which would pose a great danger to the passengers if it is not timely noticed. Three different states of the WSN and display panel in this simulation test are shown in Fig. 5(f). As the train moves regularly, the acceleration level (in cabin 3) is measured below 0.5 g with the 3rd light showing the green light. When the axial box has an acceleration value larger than 0.5 g, the 3rd light will be turned yellow by the WSN, transmitting the alarm signal to the engineers in the main control room. Once the acceleration level is detected exceeding 1.5 g, the 3rd light will be converted into red immediately to warn the engineers about the detected overload situation in cabin 3. Extending the WSN numbers and monitoring areas, the whole train can be continuously monitored to ensure a safe trip along the journey. This VR demonstration has successfully indicated the great potential of the self-sustainable WSN for diversified machine/robot monitoring applications under the IoT framework in harsh environments and remote areas. Furthermore, various self-powered gas sensors could be

integrated with our hybridized TENG and PEG vibration mechanism for toxic gas detection in harsh environments, e.g., coal mine, tunnel and chemical factory, etc [82,83].

#### 7. Conclusions

This paper proposed a self-sustainable WSN consisting of a hybrid PEG and TENG vibration module. PEG not only shows broadband vibration behavior when it impacts with TENG, but also has the frequency tuning ability by applying an axial force. The PEG has a RMS power of 6.5 mW in 1.0 g acceleration at 25 Hz as an energy harvester. A double voltage rectifier circuit is proposed to double increase voltage output of PEG. It also shows good capability in light up 30 serial LEDs in sine vibration and 20 serial LEDs in shock vibration, which can function as alarming signals in vibration and drop monitoring. Good linearity with a sensitivity of 15 V/g (0-1.5 g) has been achieved with the self-powered triboelectric accelerometer, which has an optimized separation gap of 1.5 mm. Finally, a self-sustained autonomous WSN is achieved based on a hybridized TENG and PEG vibration mechanism, with the PEG serving as the energy source and the TENG functions as the self-powered sensing unit. The feasibility of train status monitoring of the self-sustainable WSN has been demonstrated with the VR train monitoring test. Looking forward, the self-sustainable WSN as a great prospect in the eventual realization of self-sustainable monitoring systems in remote areas and harsh environments.

#### 8. Methods

#### 8.1. Preparation hybrid TENG and PEG vibration module

PMMA package is fabricated by laser cutting. Two hinged supporters are fabricated by 3D printing to hold two sides of the PZT bimorph (http: //www.pantpiezo.com). Eco flex with pyramidal synaptic array structure is made from the 3D printing mold (Fig. S6). Geometry parameters of hybrid TENG and PEG vibration modules can be found in Table S3.

#### 8.2. Vibration and power consumption test

The vibration test platform is shown in (Fig. S7). PC software sets test parameters, including sweep frequency range and vibration amplitude. Vibration controller signals are amplified by power amplifier type 2718 and then fed to the exciter WA-0308. The feedback signal is measured by an acceleration sensor CXL10GP3. The load resistance of PEG is adjusted by the resistance decade model 610. Vibration controller type 7541 also harvests voltage signals in the time domain, which are transformed into frequency domain signals through FFT changes of PC software.

The open-circuit voltage and capacitors charging curves were measured by an oscilloscope (Agilent, InfiniVision, DSO-X 3034A) and a high voltage probe (Keysight N2771B). The current consumption of WSN was tested by a power source (Otii LPA375).

#### Data availability

The data that support the findings of this study are available from the corresponding authors upon reasonable request.

# CRediT authorship contribution statement

Lu Wang: Data curation, Writing - original draft. Tianyiyi He: Revise manuscript. Zixuan Zhang: Software. Libo Zhao: Conceptualization, Methodology. Chengkuo Lee: Writing - review & editing. Guoxi Luo, Qi Mao: Visualization, Investigation. Ping Yang, Qijing Lin: Funding acquisition. Xiang Li, Ryutaro Maeda: Supervision. Zhuangde Jiang: Project administration.

# **Declaration of Competing Interest**

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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# Appendix A. Supporting information

Supplementary data associated with this article can be found in the online version at doi:10.1016/j.nanoen.2020.105555.

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